# Formation of Hydrate From Single-Phase Aqueous Solutions



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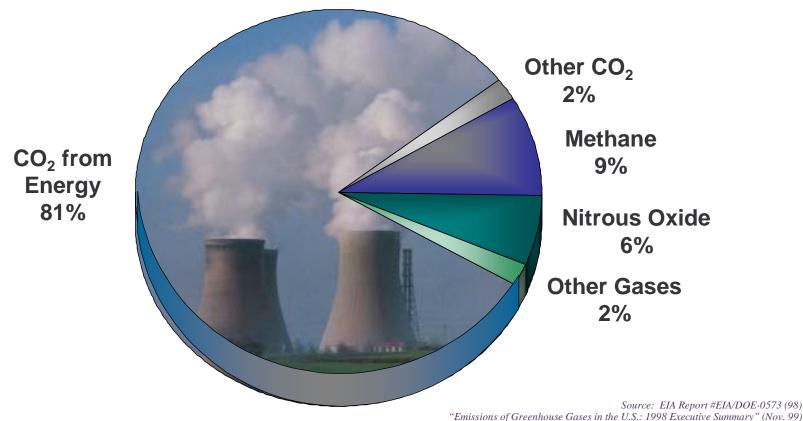
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# **CO<sub>2</sub>** from Energy is a Major Contributor to Anthropogenic Greenhouse Gas Emissions

U.S. GHG Emissions Weighted by Global Warming Potential (Equivalent Global Warming Basis)



### **Technological Carbon Management Options**

# Reduce Carbon Intensity

- Renewables
- Nuclear
- Fuel Switching

# Improve **Efficiency**

- Demand Side
- Supply Side

# Sequester Carbon

- Capture & Store
- Enhance Natural Sinks

#### All options needed to:

- Affordably meet energy demand
- Address environmental objectives

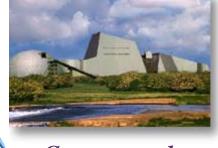




# Types of Sequestration Direct Indirect



Unmineable Coal Seams



Capture and Disposal of CO<sub>2</sub>



Deep Ocean Injection



Depleted Oil / Gas Wells, Saline Aquifers



Enhancing Natural CO<sub>2</sub> Sinks



Forestation



Iron or Nitrogen Fertilization of Ocean

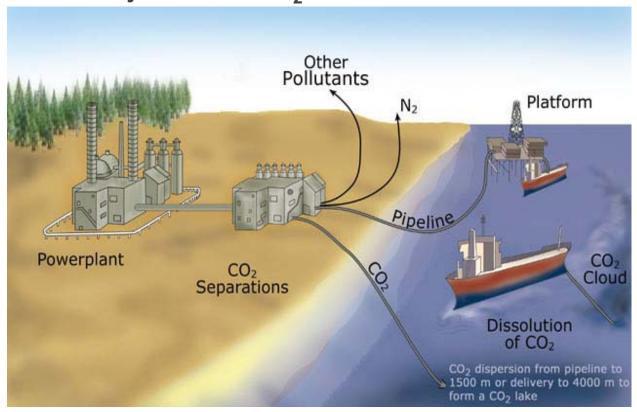


Enhanced Photosynthesis



# **Ocean Sequestration**

Direct injection of CO<sub>2</sub> into the ocean



**DOE Center for Research on Ocean Carbon Sequestration** 

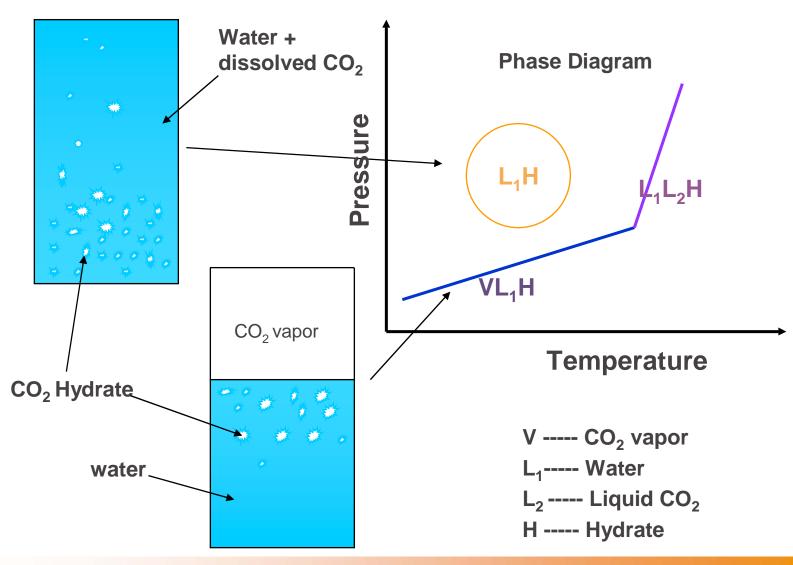


### **Implications from Previous Research**

- Physical and chemical behavior of CO<sub>2</sub> in the deep ocean, especially formation of CO<sub>2</sub> hydrate, will impact the sequestration process.
  - Hydrate formed from a <u>two-phase</u> system (liquid or gaseous CO<sub>2</sub> in contact with seawater) is initially <u>less</u> dense than seawater.
    - Rising hydrate particles reduce sequestration efficiency.
      - Greater injection depths required.
  - Hydrate formed from a <u>single-phase</u> system (CO<sub>2</sub> dissolved in seawater) is initially <u>more</u> dense than seawater.
    - Sinking hydrate particles enhance sequestration efficiency.
      - Longer CO<sub>2</sub> residence times.



### **Hydrate Formation from Single-Phase Solutions**





#### **Status of Current Research**

#### Fundamentals of hydrate formation

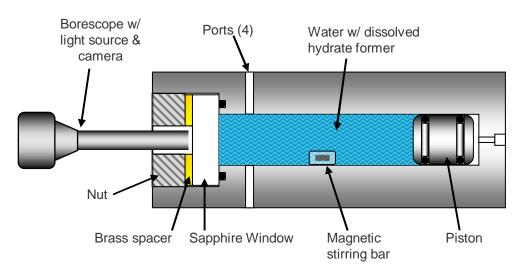
- Conducting experiments to validate thermodynamic model for predicting two-phase hydrate equilibrium (formation from singlephase aqueous solutions).
- Modifying and improving theoretical model for prediction of single-phase hydrate formation.



#### High-Pressure, Variable-Volume Viewcell

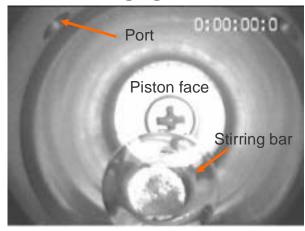
#### Features

- Direct observation of systems from 243 K to 473 K (-30°C to 200°C) at pressures to 138 MPa (20,000 psig).
- System pressure easily changed via internal piston.
- Remote monitoring and recording of observations.



High-Pressure, Variable-Volume Viewcell

#### View through glass window



General Purpose Seawater (GPS) from Ocean Scientific International, Ltd. Cell at 5.8°C, 16 MPa.



# **High-Pressure Viewcell System**



View showing syringe pumps, chamber, and computer monitoring and control system.

View showing viewcell in chamber and borescope placement.

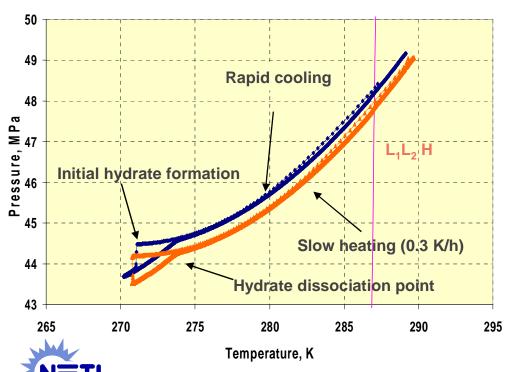




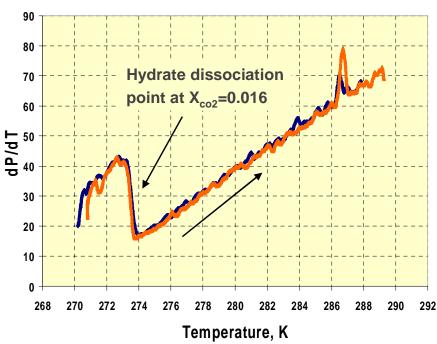
# **Experimental Data and Analysis**

 Experimental results for two cycles at X<sub>CO2</sub> = 0.016 using 18 Megohm-cm water.

Pressure vs. Temperature



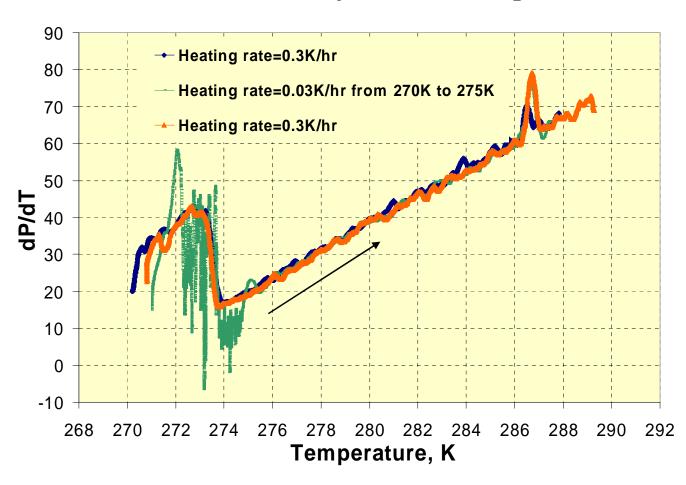
dP/dT vs. Temperature



A derivative plot permits more accurate determination of the hydrate dissociation point.

### **Examination of Heating Rate**

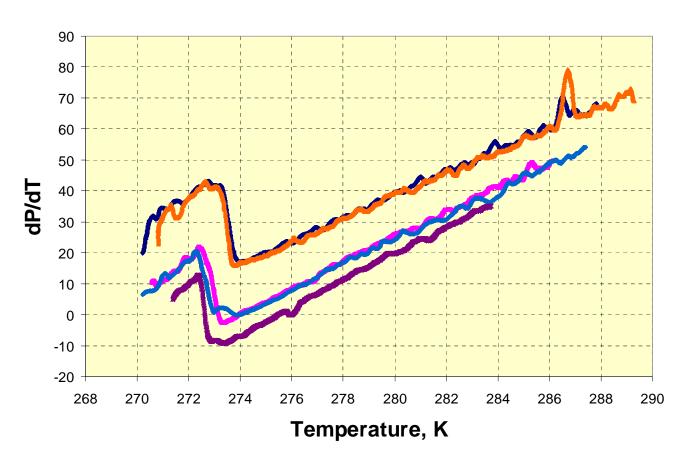
#### dP/dT vs. Temperature at Xco<sub>2</sub>=0.016





# **Comparison at Different Pressures**

dP/dT vs. Temperature at  $X_{co2}$ =0.016



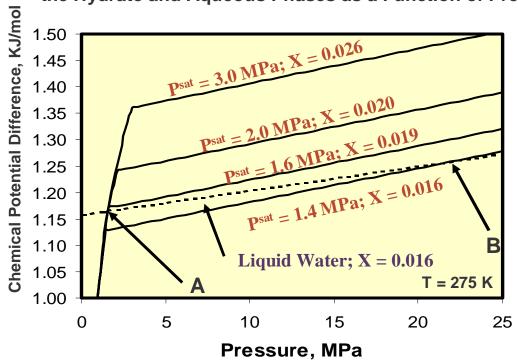


#### **Prediction of Single-Phase Hydrate Formation**

$$\frac{\Delta \mu_{H}}{RT} = -\sum_{j, cavities} v_{j} \ln \left( 1 - \sum_{i} \theta_{ji} \right) \quad \text{where,} \quad \theta_{ji} = \frac{C_{ji} f_{i}}{1 + \sum_{i} C_{ji} f_{i}}$$

$$\frac{\Delta \mu_L}{RT} = \frac{\Delta \mu_L^o}{RT_o} - \int_{T_o}^{T_F} \frac{\Delta h}{RT^2} dT + \int_{0}^{P} \frac{\Delta v}{RT} dP - \ln X_w$$

Comparison of the Chemical Potential Difference of Water in the Hydrate and Aqueous Phases as a Function of Pressure





#### **Modified Thermodynamic Model**

Hydrates form from single-phase solution, at fixed temperature

$$-\sum_{j,cavities} V_{j} \ln \left(1 - \sum_{i} \theta_{ji}\right) = \frac{\Delta \mu_{L}^{0}}{RT_{0}} + \int_{0}^{P} \frac{\Delta V}{RT} dP$$
 (1)

Hydrates form from two-phase solution, at fixed temperature

$$-\sum_{j,cavities} v_j \ln \left(1 - \sum_i \theta_{ji}^{VLH}\right) = \frac{\Delta \mu_L^0}{RT_0} + \int_0^{P^{VLH}} \frac{\Delta V}{RT} dP$$
 (2)

Subtract (2) from (1), for single hydrate species, we obtain

$$-\sum_{j,cavities} v_{j} \ln \left( \frac{1 - \theta_{ji}}{1 - \theta_{ji}^{VLH}} \right) = \int_{P^{VLH}}^{P} \frac{\Delta V}{RT} dP$$
(3)

Which gives the increase in pressure (over the VLH pressure) required to form hydrates.



### **Modified Thermodynamic Model (Cont.)**

Finally,

$$\sum_{j} V_{j} \ln \left[ \frac{\frac{1}{C_{ji} f_{i}^{VLH}} + \frac{f_{i}^{sat}}{f_{i}^{VLH}} \exp \left( \frac{V_{i} (P - P^{sat})}{RT} \right)}{\frac{1}{C_{ji} f_{i}^{VLH}} + 1} \right] = \frac{\Delta V (P - P^{VLH})}{RT}$$

$$(4)$$

– The approximations:

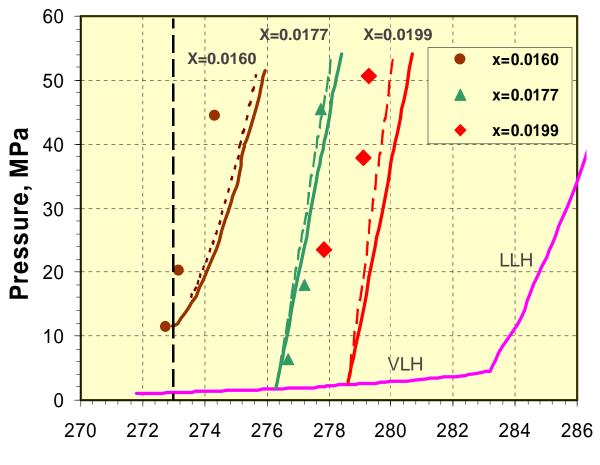
$$C_{ji}f_i^{VLH} >> 1, \qquad \frac{f_i^{sat}}{f_i^{VLH}} \approx \frac{P^{sat}}{P^{VLH}}$$

We obtain,

$$\sum_{j} v_{j} \ln \left[ \frac{P^{sat}}{P^{VLH}} \exp \left( \frac{\bar{V}_{i}(P - P^{sat})}{RT} \right) \right] = \frac{\Delta V(P - P^{VLH})}{RT}$$
 (5)



# Comparison of Experimental and Predicted Data by the Modified Model

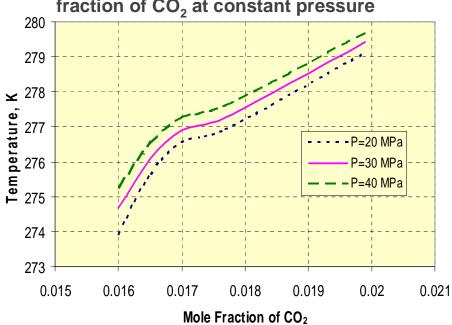


Temperature, K

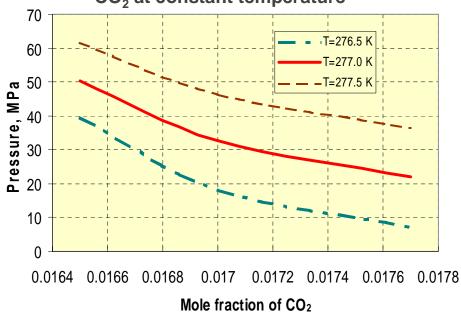
Vertical dashed line - T=273.15 K region. Solid lines - exact model; Dashed lines - simplified model

#### **Other Theoretical Calculations**

Hydrate equilibrium temperature vs. Mole fraction of CO<sub>2</sub> at constant pressure



# Pressure vs. Mole fraction of CO<sub>2</sub> at constant temperature





#### Summary

- Experimental procedures have been developed for determining the phase behavior of hydrate formed from single-phase aqueous solutions.
- A theoretical model is being developed to describe the behavior of hydrate formation from singlephase aqueous solutions.
- The results of this research will be useful in determining the efficiency and impacts of deepocean sequestration.



#### **Future Work**

#### Theoretical

- Combine "restricted rotation model" and "expanded cell model" to develop new models to provide a better understanding and prediction of the system.
- Incorporate the effect of seawater.

#### Experimental

- Complete experiments in freshwater.
- Perform experiments in seawater.





# Acknowledgement

- Ronald Lynn (NETL)
- Charles Levander (NETL)



